

## **Microwave Radiometer – 3-Channel (MWR3C) Instrument Handbook**

MP Cadeddu

February 2021



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MP Cadeddu, Argonne National Laboratory

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## Acronyms and Abbreviations

AMF	ARM Mobile Facility
ARM	Atmospheric Radiation Measurement
DQPR	Data Quality Problem Report
ENA	Eastern North Atlantic
GPS	Global Positioning System
IMMS	instrument mentor monthly summary
LNA	low-noise amplifier
LWP	liquid water path
MET	surface meteorological instrumentation
MWR	microwave radiometer
MWR3C	microwave radiometer–3-channel
MWRRET	MWR Retrievals value-added product
NetCDF	Network Common Data Form
NSA	North Slope of Alaska
OLI	Oliktok Point
PC	personal computer
PWV	precipitable water vapor
QC	quality control
REM	Rain Effect Mitigation
RMS	root mean square
RMSE	root-mean-square error
SGP	Southern Great Plains
TWP	Tropical Western Pacific
VAP	value-added product

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## 1.0 General Overview

The microwave radiometer 3-channel (MWR3C) provides time-series measurements of brightness temperatures from three channels centered at 23.834, 30, and 89 GHz. These three channels are sensitive to the presence of liquid water and precipitable water vapor.

## 2.0 Contacts

### 2.1 Mentor

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### 2.2 Vendor/Instrument Developer

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2840 Wilderness Place Unit G  
Boulder, Colorado 80301-5414  
Ph: 303-449-9192  
[info@radiometrics.com](mailto:info@radiometrics.com)

## 3.0 Deployment Locations and History

**Table 1.** Status and location of the MWR3C

Serial Number	Manufacture	Location	Date Installed	Date Removed	Status
	Radiometrics	SGP/C1	2011/10/01	2020/10/13	Retired
	Radiometrics	AMF2	2011/01/11	2017/11/09	Retired
	Radiometrics	AMF1	2012/07/25	2017/11/01	Retired
	Radiometrics	SGP/E32	2016/06/29		Operational
	Radiometrics	SGP/E41	2016/06/10	2019/03/14	Retired
	Radiometrics	SGP/E39	2016/03/31	2019/08/12	Retired
	Radiometrics	SGP/E37	2016/03/28		Operational
	RPG	ENA	2014/03/03		Operational
	RPG	OLI	2013/09/09		Operational
	RPG (G5)	AMF1	2019/10/18		Operational
	RPG (G5)	AMF2	2019/10/18		Operational
	RPG (G5)	SGP/C1	2021/01/27		Operational
	RPG (G5)	NSA/C1	2021/04		Operational

## 4.0 Near-Real-Time Data Plots

Plots of near-real-time data can be viewed at the Data Quality Explorer system accessible through the website: <http://dq.arm.gov/>. Click on “QC Metrics and Plots” and select the desired site and datastream. The MWR3C datastream is “sssmwr3cFF.b1” where ‘sss’ is the site (SGP, TWP, etc.) and ‘FF’ is the facility (C1, M1, etc.)

## 5.0 Data Descriptions and Examples

### 5.1 Data File Contents

Datastreams available from the ARM Data Center are named: sssmwr3cFF.b1 and contain calibrated brightness temperatures and retrievals. Raw data files are available upon request. For the Radiometrics systems, they are named sssmwr3cFF.00.yyyymmdd.hhmmss.raw.PR-2289C-SN\_yyyy-mm-dd\_hh-mm-ss.csv. Data files containing the calibration results from tip curves are named sssmwr3cFF.00.yyyymmdd.hhmmss.raw.PR-2289C-SN\_yyyy-mm-dd\_hh-mm-ss\_dailytips.csv. For the RPG systems, they are NetCDF files (LV0.nc).

#### 5.1.1 Primary Variables and Expected Uncertainty<sup>1</sup>

The primary variables measured by the MWR3C are brightness temperatures at 23.834, 30, and 89 GHz for the Radiometrics system and 23.8, 31.4, and 90 GHz for the RPG system. By relating the observed radiances to atmospheric water vapor and liquid water it is possible to derive precipitable water vapor (PWV) and liquid water path (LWP) from the measurements. Retrievals of integrated water vapor and liquid water path obtained from brightness temperatures measured at the three frequencies are provided in the data files. Uncertainties in the retrieved PWV and LWP are provided in the data files as individual error bars.

**Table 2.** Primary variables.

Variable Name	Quantity Measured	Unit	Uncertainty ( $1\sigma$ )
Radiometrics/Tbsky23	23.834 GHz sky brightness temperature	K	0.5 K
Radiometrics/Tbsky30	30 GHz sky brightness temperature	K	0.5 K
Radiometrics/Tbsky89	89 GHz sky brightness temperature	K	1.5 K
RPG/Tbsky23	23.8 GHz sky brightness temperature	K	0.5 K
RPG/Tbsky31	31 GHz sky brightness temperature	K	0.5 K
RPG/Tbsky90	90 GHz sky brightness temperature	K	1.5 K
lwp	Liquid water path	mm	~0.015 mm
pwv	Precipitable water vapor	cm	~0.05 cm

<sup>1</sup> See section 7.5 for a definition of uncertainty.



### 5.1.2 Secondary/Underlying Variables

**Table 3.** Secondary variables.

Variable Name	Quantity Measured	Unit	Uncertainty (1 $\sigma$ )
time	Time offset from midnight	s	
Radiometrics/RPG surface_temperature	Ambient temperature	C	0.5
Radiometrics/RPG surface_pressure	Pressure	KPa	0.1
Radiometrics/RPG surface_relative_humidity	Relative humidity	%	5
Radiometrics/ wind_direction_avg	Average wind direction	deg	3
Radiometrics/ wind_direction_max	Wind direction maximum	deg	3
Radiometrics/ wind_direction_min	Wind direction minimum	deg	3
Radiometrics/ wind_speed_avg	Average wind speed	m/s	5%
Radiometrics/ wind_speed_max	Wind speed maximum	m/s	5%
Radiometrics/ wind_speed_min	Wind speed minimum	m/s	5%
RPG (G5)/ Wind_speed	Wind speed	m/s	5%
RPG (G5)/ Wind_direction	Wind direction	deg	3
Radiometrics/RPG infrared_temperature	Zenith-pointing infrared temperature at 10 $\mu$ m	K	0.5
Radiometrics/ rain_accumulation	Rain accumulation	mm	5%
Radiometrics/ rain_duration	Rain duration	s	10
Radiometrics/RPG (G5) rain_intensity	Rain intensity	mm/hr	Not provided
Radiometrics/ hail_accumulation	Hail accumulation	hit/cm <sup>2</sup>	Not provided
Radiometrics/ hail_duration	Hail duration	s	10
Radiometrics/ hail_intensity	Hail intensity	hit/(hr cm <sup>2</sup> )	Not provided
Radiometrics/ rain_peak_intensity	Rain peak intensity	mm/hr	Not provided

### 5.1.3 Diagnostic Variables

The following diagnostic variables are in the PR-2289C-SN\_yyyy-mm-dd\_hh-mm-ss\_dailytips.csv files associated with the raw datastream for the Radiometrics systems and in the SSSmwr3ctipFF.a1.YYYYMMDD.HHMMSS.cdf for the RPG systems.

**Table 4.** Diagnostic variables.

Variable Name	Quantity Measured	Unit	Uncertainty ( $1\sigma$ )
Radiometrics/ TcaseK	Physical temperature of the K-band receiver case	K	5 K
Radiometrics/ TloadK	Physical temperature of the K-band radiometer reference load	K	5 K
Radiometrics/ TcaseW	Physical temperature of the W-band receiver case	K	1.5 K
Radiometrics/ TloadW	Physical temperature of the W-band radiometer reference load	K	2.5 K
Radiometrics/ Tnd23834	Instantaneous Tnd at 23.834 GHz from tip curves	K	0.5 K
Radiometrics/ Tnd(0C)23834	Instantaneous Tnd at 23.834 GHz at nominal temperature	K	0.5 K
Radiometrics/ TndTC23834	Temperature correction coefficient at 23.834 GHz	K/K	
Radiometrics/ Tmr23834	Mean radiating temperature at 23.834 GHz	K	10 K
Radiometrics/ R23834	Tip curve correlation coefficient		
Radiometrics/ Tnd30000	Instantaneous Tnd at 30.000 GHz from tip curves	K	0.5 K
Radiometrics/ Tnd(0C)30000	Instantaneous Tnd at 30.000 GHz at nominal temperature	K	0.5 K
Radiometrics/ TndTC30000	Temperature correction coefficient at 30.000 GHz	K/K	
Radiometrics/ Tmr30000	Mean radiating temperature at 30.000 GHz	K	10 K
Radiometrics/ R300000	Tip curve correlation coefficient		
Radiometrics/ Tnd89000	Instantaneous Tnd at 89.000 GHz from tip curves	K	2 K
Radiometrics/ Tnd(0C)89000	Instantaneous Tnd at 89.000 GHz at nominal temperature	K	2 K
Radiometrics/ TndTC89000	Temperature correction coefficient at 89.000 GHz	K/K	
Radiometrics/ Tmr89000	Mean radiating temperature at 89.000 GHz	K	10 K
Radiometrics/ R89000	Tip curve correlation coefficient		
RPG/ tndmed23	Median Tnd at 23 GHz	K	0.5 K
RPG/ Tndinst23	Instantaneous Tnd at 23.000 GHz from tip curves	K	2 K
RPG/ r23	Tip curve correlation coefficient at 23 GHz		
RPG/ Mean_rad_temp_23	Mean radiating temperature at 23.000 GHz	K	10 K
RPG/ Tndmed31	Median Tnd at 31 GHz	K	0.5 K

Variable Name	Quantity Measured	Unit	Uncertainty (1 $\sigma$ )
RPG/ Tndinst31	Instantaneous Tnd at 31.000 GHz from tip curves	K	2 K
RPG/ R31	Tip curve correlation coefficient at 31 GHz		
RPG/ Mean_rad_temp_31	Mean radiating temperature at 31.000 GHz	K	10 K
RPG/ Tndmed90	Median Tnd at 90 GHz	K	0.5 K
RPG/ Tndinst90	Instantaneous Tnd at 90.000 GHz from tip curves	K	2 K
RPG/ R90	Tip curve correlation coefficient at 90 GHz		
RPG/ Mean_rad_temp_90	Mean radiating temperature at 90.000 GHz	K	10 K
RPG (G5)/ gain_23	23.84 GHz channel gain	V/K	N/A
RPG (G5)/ gain_31	31.4 GHz channel gain	V/K	N/A
RPG (G5)/ gain_90	90 GHz channel gain	V/K	N/A
RPG (G5)/ trec_23	23.84 GHz channel gain	K	N/A
RPG (G5)/ trec_31	31.4 GHz channel gain	K	N/A
RPG (G5)/ trec_90	90 GHz channel gain	K	N/A

### 5.1.4 Data Quality Flags

Data quality flags are named qc\_‘fieldname’ (i.e., qc\_tbsky90). Possible values for qc\_flags are: 0 (value is within the specified range), 1 (missing value), 2 (value is less than the specified minimum), 4 (value is greater than the specified maximum), and 8 (value failed the valid “delta” check). Specified maximum and minimum values are shown in Table 5.

**Table 5.** Data quality thresholds.

Field Name	Min	Max
Radiometrics/Tbsky23	2.73	330
Radiometrics/Tbsky30	2.73	330
Radiometrics/Tbsky89	2.73	330
Radiometrics/surface_temperature	-50	50
Radiometrics/surface_pressure	70	110
Radiometrics/surface_relative_humidity	0	110
Radiometrics/wind_direction_avg	0	360
Radiometrics/wind_direction_max	0	360
Radiometrics/wind_direction_min	0	360

Field Name	Min	Max
Radiometrics/wind_speed_avg	0	30
Radiometrics/wind_speed_max	0	30
Radiometrics/wind_speed_min	0	30
Radiometrics/infrared_temperature	173	305
Radiometrics/rain_accumulation	0	30
Radiometrics/rain_duration	0	21600
Radiometrics/rain_intensity	0	500
Radiometrics/hail_accumulation	0	10
Radiometrics/hail_duration	0	3600
Radiometrics/hail_intensity	0	500
Radiometrics/rain_peak_intensity	0	30
RPG/Tbsky23	2.73	330
RPG/Tbsky31	2.73	330
RPG/Tbsky90	2.73	330
RPG/surface_temperature	-50	50
RPG/surface_pressure	70	110
RPG/surface_relative_humidity	0	110

### 5.1.5 Dimension Variables

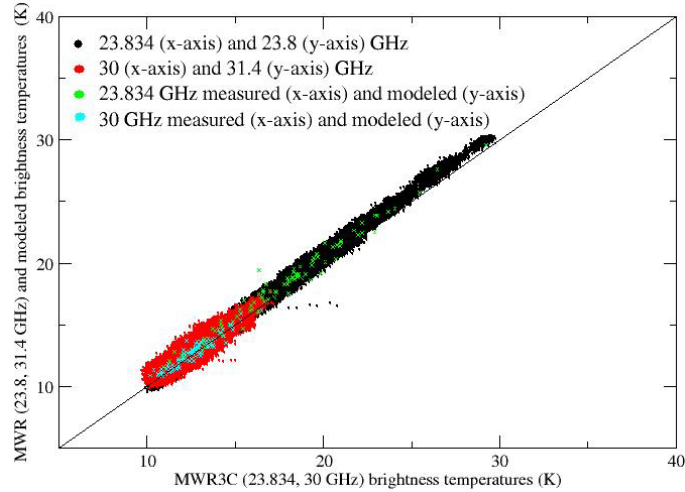
These variables are common to the Radiometrics and RPG systems.

**Table 6.** Dimension variables.

Field Name	Quantity	Unit
base_time	Base time in Epoch	seconds since 1970-1-1 0:00:00 0:00
time_offset	Time offset from base_time	s
lat	north latitude	degrees
lon	east longitude	degrees
alt	altitude	meters above Mean Sea Level

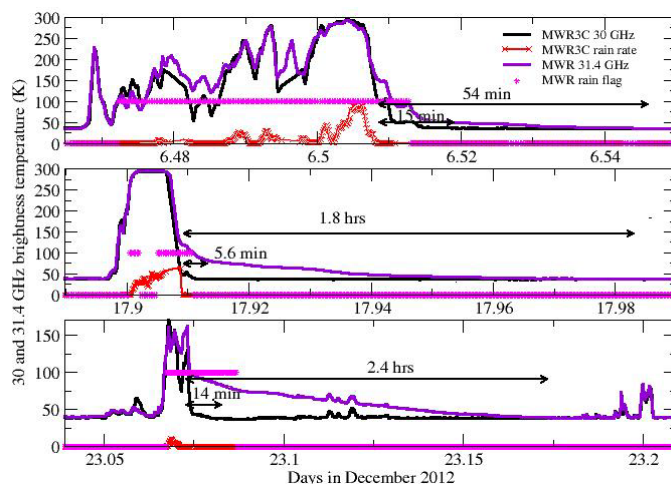
## 5.2 Annotated Examples

In this section are some examples of data. Figure 1 (1) shows a comparison of brightness temperatures between the microwave radiometer (MWR) and the MWR3C at the Southern Great Plains (SGP) site for the month of November 2011. The figure shows a very good consistency of the measurements from the two instruments. For the example shown the root-mean-square (RMS) differences between measured and modeled brightness temperatures (green points) are 0.7 K and 0.4 K for the 23.834 and 30 GHz respectively. The slightly higher RMS differences in the 23.834 GHz channel may be due to a residual temperature dependence of the calibration of that channel.



**Figure 1.** Brightness temperatures measured by the MWR3C at 23.834 and 30 GHz (black and red) versus MWR measurements at 23.8 and 31 GHz (y-axis). Green and cyan points are brightness temperatures at 23.834 and 30 GHz measured by the MWR3C (x-axis) and modeled (y-axis). Data were collected at the SGP during the month of November 2011. Figure from (1).

The rain mitigation system is designed to keep the two receivers' lenses dry in situations of high humidity or light rain. For this purpose a stream of warm air is blown across the lenses when the relative humidity exceeds a user-adjustable threshold. Air is blown at high speed during rain to keep the lenses clear of standing water. The rain detection and mitigation system of the MWR3C shows improved capability in quickly drying the lenses after a rain event as shown in Figure 2 (1). The three panels show brightness temperatures (30 GHz) during three rain events on Gan Island, Maldives, in December 2011. Red crosses indicate rain rate (mm/hr) as reported by the MWR3C rain sensor. Pink crosses indicate the times when the MWR rain flag was on (100) and off (0). During these times the heater in the MWR dew blower was blowing warm air on the radiometer's Teflon window. The two black lines with arrows start when the rain stops (according to the MWR3C sensor). In general the MWR3C brightness temperatures drop back to normal levels after approximately 5-10 minutes from the end of the rain, suggesting that this is the time necessary to completely free the lens of standing water.



**Figure 2.** Three rain events on Gan Island, Maldives and the effect of the rain mitigation system on the MWR (violet line, 31.4 GHz) and the MWR3C (black line, 30 GHz). Red points are the rain rate (mm/hr) measured by the MWR3C weather station; pink points represent the times when the MWR rain flag was on. The black solid lines indicate the time between the end of the rain (zero rain rate according to the MWR3C) and the return of brightness temperatures to approximate pre-rain values. Figure from (1).

### 5.3 User Notes and Known Problems

Starting in June 2018 the E32 unit has intermittent data from the surface meteorological instrumentation (MET) sensor (see DQPR 7158).

### 5.4 Frequently Asked Questions

This section is not yet available.

## 6.0 Data Quality

### 6.1 Data Quality Health and Status

Daily quality check on this datastream can be found at the Data Quality Explorer page: <http://dq.arm.gov/>. Click on “QC Metrics and Plots” and select the desired site and datastream. For example, for the MWR3C located at the site “SGP”, the datastream is “sgpmwr3cC1.b1” and the facility is “C1”.

### 6.2 Data Reviews by Instrument Mentor

The instrument mentor submits a monthly summary report (instrument mentor monthly summary: IMMS) accessible from the instrument web page. Some of the general checks performed by the instrument mentor are described below.

1. In general, the brightness temperature time series should be smooth and with low noise levels.
2. Brightness temperatures should be greater than 2.75 K and less than approximately 330 K.

3. External temperature readings can be compared to tower measurements. The agreement should be +/- 2 K.
4. External pressure readings can be compared to tower measurements. The agreement should be +/- 5 KPa.
5. External relative humidity readings can be compared to tower measurements. The agreement should be +/- 5%
6. Measured brightness temperatures are also compared with model computations as a general quality check.
7. Data from the rain detection system are routinely checked against other similar measurements depending on their availability at a given site.

## **6.3 Data Assessments by Site Scientist/Data Quality Office**

The Data Quality office daily data assessment can be view at the DQHands web page.

## **6.4 Value-Added Procedures**

The MWR Retrievals (MWRRET) algorithm provides physical retrievals of water vapor and liquid water path.

# **7.0 Instrument Details**

## **7.1 Detailed Description**

The Radiometrics MWR3C measures sky radiances at three frequencies: 23.834, 30, and 89 GHz. Radiance measurements are converted to “equivalent brightness temperatures” through the calibration procedure.

The RPG MWR3C measures sky radiances at three frequencies: 23.8, 31, and 90 GHz. Radiance measurements are converted to “equivalent brightness temperatures” through the calibration procedure.

Below is detailed description of the instrument components for each system.

### **7.1.1 List of Components**

Radiometrics:

- RF section: 2 microwave receivers PR2289 model manufactured by Radiometrics Corp.
- FLIR DP300 pan tilt unit
- Main junction box
- Embedded PC controller
- Radiometer stand

- Rain Effect Mitigation (REM) system composed of a blower assembly and 2 heaters
- Vaisala weather station WXT510
- Garmin GPS unit
- Heitronix KT15II infrared thermometer

RPG:

- RF section: 2 microwave receivers
- PC
- Radiometer stand
- Blower assembly
- Vaisala weather station
- infrared thermometer

## **7.1.2 System Configuration and Measurement Methods**

### **7.1.2.1 Radiometrics**

In this section we briefly describe the MWR3C hardware configuration. The MWR3C is composed of two PR-series microwave receivers. The PR2230 is the K-band receiver and can be calibrated to up to 30 frequencies between 22 and 30 GHz. In operational mode only 2 channels (22.834 and 30 GHz) are calibrated. The K-band channels have a bandwidth of 300 MHz. The PR8900 is the W-band receiver that is calibrated at 89 GHz (1.9 GHz bandwidth). The receivers are enclosed in a watertight case equipped with active moisture and pressure control. The entire receiver subsystem with the exception of the external lens is thermally stabilized to 30 mK. Residual temperature dependences due to the external lens are corrected in the calibration procedure with the use of additional temperature coefficients. The radiation entering the lens passes through a feedhorn and is directed to a PIN switch. The switch is periodically set to a load position. In this case the receiver sees the “black body” that is kept at a temperature carefully monitored with a precision thermometer. The gain is monitored by periodically injecting a calibrated noise through a noise diode. The receivers are moved in azimuth and elevation by a pan tilt unit and they are equipped with internal accelerometers to precisely determine the elevation angle. In normal operation mode the radiometers observe the sky in zenith position. Zenith measurements are interrupted approximately every 15 minutes to collect scanning measurements used to perform the absolute calibration. All data processing and software operations are performed by an embedded computer located inside the main junction box.

The two receivers’ lenses are kept free of dew and water drops in drizzle conditions by the Rain Effect Mitigation (REM) system. The system is composed of a dew blower and two heaters that blow warm air on the lenses when the relative humidity exceeds a user-selectable threshold.



### 7.1.2.2 RPG

The material in this section can be found in (1). The radiometer has two direct-detection receiver units. An off-axis paraboloid mirror is used to focus microwave radiation onto a corrugated feed horn. The microwave radiation entering the instrument is first decomposed into two beams. Each beam is directed in a feed horn to generate a beam of the desired divergence ( $\sim 3.3^\circ$  and  $1.6^\circ$  HPBW). A 40-dB low-noise amplifier (LNA) boosts the input signal before it is filtered and boosted again by another 20-dB amplifier. The waveguide band pass filters bandwidths and center frequencies are listed in Table 7. All channels are detected and integrated simultaneously. The receivers are based on the direct detection technique, where the signal is directly amplified, filtered, and detected.

The radiometer receivers are thermally stabilized to an accuracy of  $\pm 0.02$  K. Due to this extremely accurate stability, the instrument can run without gain calibration for about 30 minutes maintaining a radiometric accuracy of  $\pm 0.3$  K. The systems labeled as G5 have a continuous gain calibration and are calibrated with RPG proprietary methodology.

### 7.1.3 Specifications

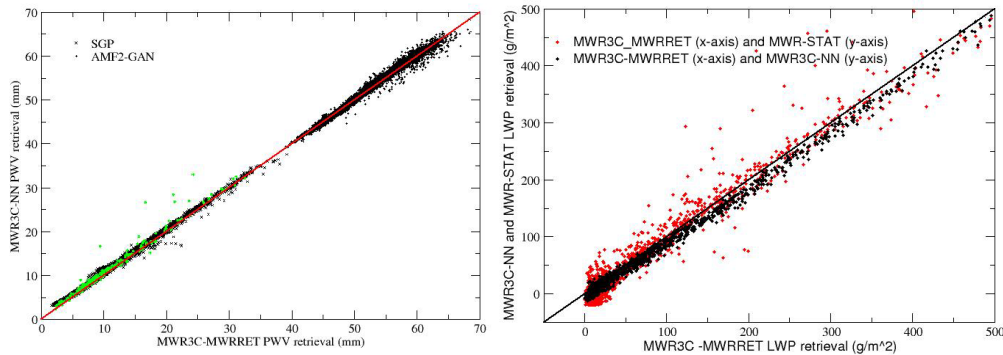
**Table 7.** Instrument specifications.

Parameter	Value
Radiometrics/ Receiver noise temperature 23.834 GHz	< 500 K
Radiometrics/ Receiver noise temperature 30 GHz	< 500 K
Radiometrics/ Receiver noise temperature 89 GHz	<1100
Radiometrics/ Channel bandwidth K-band	300 MHz
Radiometrics/ Channel bandwidth W-band	1900 MHz
Radiometrics/ Radiometric resolution	0.4 K RMS@1 s integration time
Radiometrics/ Receiver and antenna thermal stabilization	< 30 mK (excluded external lens)
Radiometrics/ Integration time	$\geq 1$ s
Radiometrics/ HPBW K-band channels	$\sim 3.0^\circ$
Radiometrics/ HPBW W-band channel	$\sim 3.5^\circ$
Radiometrics/ Temperature range	-40 to +45 C (environmental chamber tested)
RPG/ Receiver noise temperature 23.8 GHz	< 400 K
RPG/ Receiver noise temperature 31 GHz	< 400 K

Parameter	Value
RPG/ Receiver noise temperature 90 GHz	<800
RPG/ Channel bandwidth K-band	230 MHz
RPG/ Channel bandwidth W-band	2000 MHz
RPG/ Radiometric resolution	0.4 K RMS@1 s integration time
RPG/ Receiver and antenna thermal stabilization	< 30 mK (excluded external lens)
RPG/ Integration time	>=1 s
RPG/ HPBW K-band channels	~3.0°
RPG/ HPBW W-band channel	~1.6
RPG/ Temperature range	-40 to +45 C (environmental chamber tested)

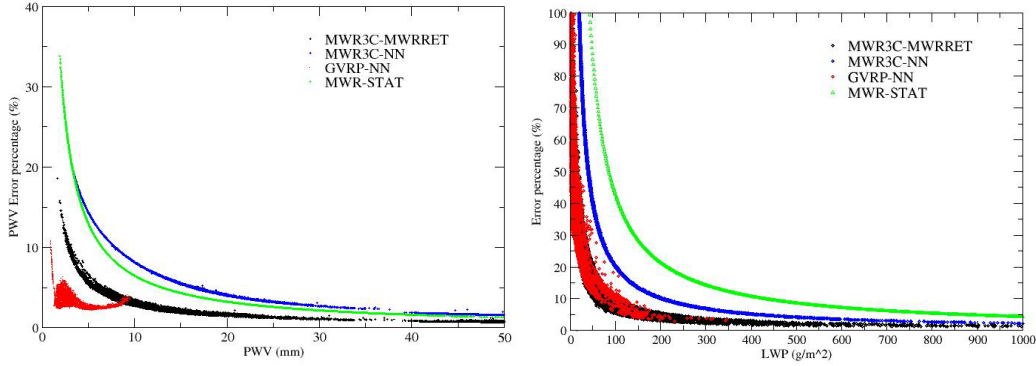
## 7.2 Theory of Operation

The three channels of the MWR3C are highly sensitive to the presence of water vapor and liquid water in the atmosphere. The two K-band frequencies (23.834 and 30 GHz, or 23.8 and 31 GHz) are similar to the frequencies sampled by the MWR (23.8 and 31.4 GHz) to ensure continuity of the measurements. The additional 89 (or 90) GHz channel provides increased sensitivity to the presence of cloud liquid water. The additional channel should therefore improve LWP retrievals, particularly when the liquid water amount is low. Real-time retrievals of integrated water vapor and liquid water path are available from the ARM Data Center in the datastream sssmwr3cFF.b1. The retrievals are obtained with a neural network algorithm similar to the one described in (2). Physical retrievals are available as value-added products (VAPs). Figure 3 (left panel, [1]) shows a comparison of PWV retrieved with the neural network and the physical retrieval at the SGP and at the AMF2-GAN. The right panel shows LWP retrievals.



**Figure 3.** Left panel: comparison of PWV retrievals from the MWR3C physical (x-axis) and neural network (y-axis) retrievals (1). At the SGP (crosses) and AMF2-GAN (circles). Green points represent radiosondes measurements. Right panel: LWP retrievals from the MWR3C physical (x-axis) and neural network (y-axis, black) retrievals. Red points are the MWR statistical retrievals.

With the addition of the 89 (90)-GHz channel, the PWV and LWP retrieval uncertainty can be reduced as shown in Figure 4 (1).



**Figure 4.** Left panel: Percentage PWV error as a function of PWV from various instruments and algorithms. Right panel: same as in the left panel but for LWP retrieval. Figure from (1).

## 7.3 Calibration

### 7.3.1 Theory

Once in the field, the MWR3C calibrates exclusively with tip curves. In-factory calibration determines the receiver non-linearity coefficients and the lens temperature-dependent offset. A residual temperature dependence of the lens is derived from the tip curves results in the Radiometrics systems. With the tip curve algorithm, the gain and receiver temperature are uniquely determined. The processing of the tip curves is designed to be consistent with the MWR's (3) and MWRHF's (1) calibration procedures. Tip curves are collected every 15 minutes. In the tip curve procedure a linear regression is performed between the optical thickness and the air mass. The straight line is extrapolated to zero air mass. The detector reading at this point corresponds to a radiometric temperature, which equals the system noise temperature plus 2.7 K. A second detector voltage is measured with the radiometer pointing at the ambient temperature with known radiometric temperature. Various corrections are applied to achieve increased accuracy in the results. Once a sufficiently large number of acceptable tip curves are collected (the number of points as well as the acceptance criterion are user selectable), they are processed and a median value is used in the computations of brightness temperatures.

### 7.3.2 Procedures

The calibration algorithm is based on the assumption that, although noise diodes are known to be stable over time, the effective noise diode injection temperature as determined from tip curves will eventually show some drift over a period of a few months. For the **Radiometrics** systems the radiometer equations used to calibrate the brightness temperatures are the following:

$$v_{load} = G(T_{rcv} + T_{load} + Offset)^{\alpha} \quad (1)$$

$$v_{loadND} = G(T_{rcv} + T_{load} + Offset + T_{ND})^{\alpha} \quad (2)$$

$$v_{sky} = G(T_{rcv} + T_{sky})^{\alpha} \quad (3)$$

Where  $V_{load}$  and  $V_{loadND}$  are detector voltages recorded when viewing the internal reference load with the noise diode off and on and  $V_{sky}$  are voltages recorded when viewing the sky. The noise diode injection temperature  $T_{ND}$  and the *Offset* have a residual temperature dependence:

$$T_{ND} = T_{ND}^0 + c_1 T_c \quad (4)$$

$$Offset = Offset^0 + c_2 T_c \quad (5)$$

Where  $T_{ND}^0$  and  $Offset^0$  are the values at the nominal temperature of 0° C,  $c_1$  and  $c_2$  are coefficients, and  $T_c$  is the physical temperature of the receiver case expressed in degrees Celsius. The gain is therefore expressed as:

$$G = \left( \frac{V_{loadND}^{1/\alpha} - V_{load}^{1/\alpha}}{T_{nd}} \right)^\alpha \quad (6)$$

and the receiver temperature  $T_{rcv}$  as:

$$T_{rcv} = \left( \frac{v_{load}}{g} \right)^\alpha - T_{load} - Offset. \quad (7)$$

The sky temperature is computed as:

$$T_{sky} = \left( \frac{v_{sky}}{g} \right)^{1/\alpha} - T_{rcv}. \quad (8)$$

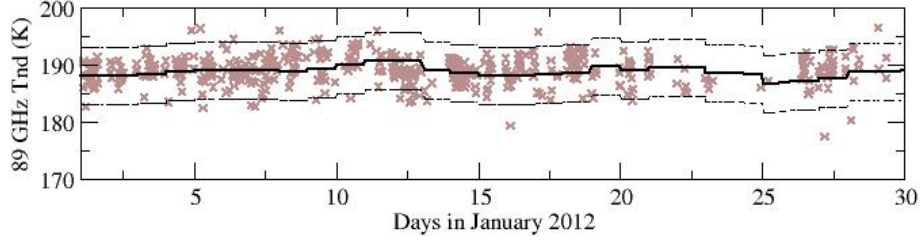
Equation 8 is the basic equation that is used in the calibration. The gain is monitored at each measurement point. On the other hand the noise diode is calibrated with the tip curves procedure. During tip calibrations the radiometer scans on both sides of the window and also acquires readings of the internal load. The noise diode is calibrated with the following equation:

$$T_{ND} = \left( \frac{\frac{1}{v_{loadND}^\alpha} - \frac{1}{v_{load}^\alpha}}{\frac{1}{v_{sky}^\alpha} - \frac{1}{v_{load}^\alpha}} \right) (T_{sky} - T_{skyload} - Offset). \quad (9)$$

To have an estimate of  $T_{ND}$  it is necessary to acquire an independent  $T_{sky}$  value. This is achieved through frequent tip curves. In the tip curve procedure the opacity ( $\tau$ ) computed at each elevation angle is plotted as a function of airmass and the slope of the regression ( $\tau_z$ ) is computed.  $T_{sky}$  is then determined as:

$$T_{sky} = T_{bg} e^{-\tau} + T_{mr} (1 - e^{-\tau}). \quad (10)$$

where  $T_{mr}$  is the atmospheric mean radiating temperature. This  $T_{sky}$  value is then substituted in (9) to determine the *instantaneous* value of  $T_{nd}$ . Instantaneous values of  $T_{nd}$  are collected and stored. Once a day the algorithm processes the acquired tip curves and determines a median value that is used in (6) and (8). An example of estimated  $T_{ND}$  for the 89 GHz channel is shown in Figure 5 (from [1]).



**Figure 5.** Instantaneous  $T_{nd}$  values derived from tip curves (brown points) and running median values (black line). The dashed lines represent 2 standard deviations from the mean.

**The RPG (not labeled as G5)** system is calibrated similarly to the MWRHF. The radiometer equation used in the algorithm is:

$$T_{sky} = T_{bb} + (V_{sky} - V_{bb})/G \quad (11)$$

where  $V_{sky}$  is the signal recorded when the reflector is oriented towards the sky,  $V_{bb}$  is the signal recorded while looking at the black body target,  $G$  is the gain, and  $T_{bb}$  is the physical temperature of the black body target. Equation 11 is the basic equation used in the calibration. The radiometer performs absolute calibrations by conducting tip curves every hour and gain calibrations every 5 minutes. During tip calibrations the radiometer scans on both sides of the window and acquires black body readings. During gain calibration the radiometer acquires only black body readings.

The gain  $G$  is determined by:

$$G = \frac{V_{bb+nd}^\alpha - V_{bb}^\alpha}{T_{nd}} \quad (12)$$

where  $V_{bb+nd}$  is the signal associated to the black body with the noise diode on.

To have an estimate of  $T_{nd}$  it is necessary to acquire an independent  $T_{sky}$  value. This is achieved through hourly tip curves as previously described. This  $T_{sky}$  value is then substituted in (3) to determine the *instantaneous* value of  $T_{nd}$  that will be called  $T_{ndI}$  (9). Scanning on both sides of the window, although it increases the time necessary for the calibration, helps to minimize the errors due to misalignment. Notice that only the slope (and not the intercept) is determined in the tip curve process. A tip curve is considered good if the correlation coefficient of the regression is higher than a predefined threshold of 0.995. The variability in the instantaneous values  $T_{ndI}$  is such that it is not desirable to introduce these single values directly in the calibration algorithm (2) and (1). Instead, the following procedure is adopted: Instantaneous values  $T_{ndI}$  are collected and stored in a circular array of 50 (or more) points and the median value of the array is computed. Every time a new tip is collected, the elements of the array are shifted one position and the newest tip is stored as the last element of the array. A new median value of the array is then computed.

The brightness temperature is calculated from the calibrated gain as:

$$TB_{sky} = \left( \frac{v_{sky}}{G} \right)^\alpha - T_{sys} \quad (13)$$

where

$$T_{sys} = \left(\frac{v_{bb}}{G}\right)^\alpha - T_{bb}.$$

The systems labeled as **RPG G5** follow a RPG proprietary calibration that involves continuous calibration with noise diode.

### 7.3.3 History

2009-2011: Initial tests, design modification, and REM system development.

2011: Deployment of first three operational units at the AMF2, SGP, TWP C3.

## 7.4 Operation and Maintenance

### 7.4.1 User Manual

User manuals are provided to the site operators during the deployment stage.

### 7.4.2 Routine and Corrective Maintenance

To be written.

### 7.4.3 Software Documentation

Available through the Data Management Facility or instrument mentor.

### 7.4.4 Additional Documentation

N/A

## 8.0 Glossary

**Uncertainty:** We define uncertainty as the range of probable maximum deviation of a measured value from the true value within a 95% confidence interval. Given a bias (mean) error  $B$  and uncorrelated random errors characterized by a variance  $\sigma^2$ , the root-mean-square error (RMSE) is defined as the vector sum of these:

$$RMSE = (B^2 + \sigma^2)^{1/2}.$$

( $B$  may be generalized to be the sum of the various contributors to the bias and  $\sigma^2$  the sum of the variances of the contributors to the random errors). To determine the 95% confidence interval we use the Student's  $t$  distribution:  $t_{n,0.025} \approx 2$ , assuming the RMSE was computed for a reasonably large ensemble. Then the *uncertainty* is calculated as twice the RMSE.

## 9.0 Acronyms

See <https://arm.gov/resources/acronyms>

## 10.0 References

- (1) Cadeddu, MP, JC Liljegren, and DD Turner. 2013. “The atmospheric radiation measurement (ARM) program network of microwave radiometers: Instrumentation, data, and retrievals.” *Atmospheric Measurement Techniques* 6(9): 2359–2372, <https://doi.org/10.5194/amt-6-2359-2013>
- (2) Cadeddu, MP, DD Turner, and JC Liljegren, 2009. “A neural network for real-time retrievals of PWV and LWP from arctic millimeter-wave ground-based observations.” *IEEE Transactions on Geoscience and Remote Sensing* 47(7): 1887–1900, <https://doi.org/10.1109/TGRS.2009.2013205>
- (3) Liljegren, JC. 2000. “Automatic self-calibration of ARM microwave radiometers,” in *Microwave Radiometry and Remote Sensing of the Earth’s Surface and Atmosphere*, P. Pampaloni and S. Paloscia, Eds. VSP Book, Lorton, Virginia, pp. 433–443.
- (4) RPG\_MWR\_STD\_Technical\_Manual\_2015 available for download from [https://www.radiometer-physics.de/downloadftp/pub/PDF/Radiometers/General\\_documents/Manuals/2015/RPG\\_MWR\\_STD\\_Technical\\_Manual\\_2015.pdf](https://www.radiometer-physics.de/downloadftp/pub/PDF/Radiometers/General_documents/Manuals/2015/RPG_MWR_STD_Technical_Manual_2015.pdf)



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